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List of Occupant Injury Criteria

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16. Abstract

This study constitutes a summary literature review of injury criteria currently used by regulatory agencies (aerospace and automotive) worldwide, and presents state-of-the-art injury criteria and associated research for most body regions. The literature review findings have been divided into two categories: state-of-the-art injury criteria and state- of- the- art injury research. The state-of-the-art injury criteria category collects those documents where injury criteria are well defined and includes adequate tolerance limits for the criterion in question. This injury criterion should be measurable or derived from physical test parameters. On the other hand, the papers documented as state-of-the-art injury research include those criteria that were or are currently being developed but do not have well defined limits or cannot be measured from physical test parameters.

The study divides injury criteria into classifications of: head, neck, torso, upper extremities, and lower extremities. Each body region is then divided into sagittal and coronal loading. Sagittal and coronal loading are subdivided into existing-regulatory, state-of-the-art injury criteria, and state-of-the-art injury research according to the previous definitions.

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LIST OF ACRONYMS

AUROC Area under receiving operating characteristic (ROC) curve

BRIC Kinematic rotational brain injury criterion

AIS Abbreviated injury scale
ATD Anthropomorphic test device

BC Blunt criterion

BrIC Brain injury criterion Contribution factor

C_{max} Maximum chest deflection CFR Code of federal regulations

CP Combined probability of concussion CSDM Cumulative strain damage measure

CSF Cerebral spinal fluid

CTI Combined thoracic injury criterion

d₁ Maximal deflection caused by localized loading

DAI Diffuse axonal injury dD Differential deflection

d_d Maximal deflection caused by the distributed loading

d_{eq} Equivalent deflectionDs Sternal deflection

ECE Economic Commission for Europe FAA Federal Aviation Administration

FE Finite Element

FEA Finite Element Analysis
FFC Femur force criterion
fn Normalization factor
GSI Gadd severity index
HIC Head injury criterion

HIC36 Head injury criterion in a 36ms interval

HIP Head injury power

IARV Injury assessment reference value
IIHS Insurance Institute for Highway Safety
IV-NIC Intervertebral neck injury criterion

KTH Knee-thigh-hip
Lc Characteristic length
LIN Linear accelerations
LNL-index Lower neck load index

MANIC(Gy)Multi-axial neck injury criterion

MIX Mix criterion

mTBI Mild traumatic brain injury

N/A Not Applicable

NCAP New car assessment program NDC Neck displacement criterion

NHTSA National Highway Traffic Safety Administration

NIAR National Institute for Aviation Research

NIC Neck injury criterion NII Neck injury index

NII_{PMHS} Adaptation of NII based on PMHS tests

N_{ij} Neck injury criterion for frontal impact

N_{km} Neck protection criterion

OC Occipital condyle

PCS Principal Component score PMHS Post Mortem Human Subject

PRHIC Power rotational head injury criterion

RIC Rotational injury criterion

ROC Receiver operating characteristic

ROT Rotational accelerations
SDH Subdural hematoma
SFC Skull fracture correlate

SSD Sum of shearing displacements

T1-vertebra First thoracic vertebra TBI Traumatic brain injury

TCFC Tibia compression force criterion ThCC Thoracic compression criterion

TI Tibia index

TTI Thoracic trauma index ULP Universit'e Louis Pasteur

VC Viscous criterion

VM Von-Mises

WAD Whiplash associated disorder WIC Whiplash injury criterion

LIST OF OCCUPANT INJURY CRITERIA

INTRODUCTION

The Federal Aviation Administration (FAA) defines the requirements for occupant protection during emergency landing dynamic conditions in 14 Code of Federal Regulation (CFR) Parts §2x.562. Parts §2x.785 also mentions that the occupant should not suffer serious injury in an emergency landing condition as specified in 2x.562. These CFRs apply to all seats regardless of orientation. However, other occupant protection requirements are usually imposed on side and oblique-facing seats. The current safety criteria specified in these CFRs only include head, pelvis, and femur loading (Part 25 only). The current report includes a comprehensive list of regulatory and state-of-the-art injury criteria for most body regions. These can aid in identifying new guidelines for occupant safety under sagittal and/or coronal loading. This report does not encompass all injury criteria available but it is meant to provide some of the state-of-the-art injury criteria and research publicly available.

The three anatomical body-plane regions are comprised of the sagittal, coronal, and transverse plane. Figure 1 highlights the three anatomical planes. Sagittal loading typically occurs during a frontal impact (forward and aft-facing seats). Motion in the coronal plane occurs when the occupant goes side-to-side. This typically occurs in a side impact (for a forward-facing seat) or when the occupant is seated in a side-facing seat (for a fore-aft crash). Loading due to a vertical impact occurs in both the sagittal and coronal planes.

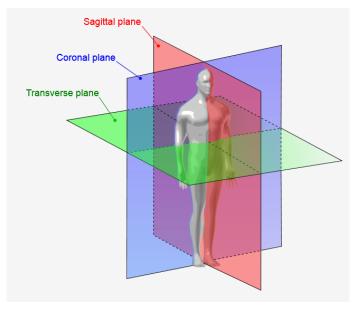


Figure 1. Anatomical Planes [1]

The literature review findings have been divided into three categories: regulatory, state-of-the-art injury criteria, and state-of-the-art injury research. Regulatory injury criteria are those currently used to assess occupant injury levels such as the Head Injury Criteria (HIC) in 14 CFR Part 25.562. The state-of-the-art injury criteria category collects those documents where injury criteria are well defined and includes adequate tolerance limits for the criterion in question. This injury criterion should be measurable or derived from physical test parameters. On the other hand, the papers documented as state-of-the-art injury research include those criteria that were or are currently being developed but do not have well defined limits or cannot be measured from physical test parameters (i.e. Von-Mises stress of a specific part of the brain). Criteria applicable to vertical loading were only included for the lumbar spine.

The results are organized by body region: head, neck, torso, upper extremities, and lower extremities. Each body region is then divided into sagittal and coronal loading. Sagittal and coronal loading are subdivided into existing-regulatory, state-of-the-art injury criteria, and state-of-the-art injury research according to the previous definitions. The nomenclature for each region is comprised of four variables. The first variable identifies the body region, i.e., H for the head, N for the neck, etc. The second variable specifies the type of impact injury, such as penetrating (P) or blunt (B). The third variable is either one or two lower case letters that identify the type of criterion; regulatory (r), state-of-the-art injury criterion (ac), or state-of-the-art injury research (ar). The last variable is a numerical value to keep track of the criteria within the groups and subgroups. Figure 2 shows an example of one of the cases of the head nomenclature.

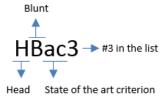


Figure 2. Nomenclature example

INJURY CRITERIA FOR THE HEAD

SAGITTAL LOADING

Regulatory

Table 1 provides a summary of blunt injury criteria for the head currently in use by regulatory agencies.

Table 1. Injury criteria for the head under blunt sagittal loading – regulatory

Criterion Nomenclature	Injury Criterion	Agencies
HBr1	HIC HIC = 390 to 1000 (depending on version and regulation)	FAA [2] NHTSA [3] ECE [4] Japan NCAP [5] IIHS [6] Euro NCAP [7]
HBr2	Deceleration of head form cannot exceed 80g for more than 3ms	NHTSA [3] ECE [4] Euro NCAP [7]

Table 2 provides a summary of penetrating injury criteria for the head currently in use by regulatory agencies.

Table 2. Injury criteria for the head under penetrating sagittal loading – regulatory

Criterion Nomenclature	Injury Criterion	Agencies
HPr1	Areas of contact free of protrusions or sharp edges	FAA [8] NHTSA [9]

State-of-the-Art Injury Criteria

Table 3 provides a summary of sagittal state-of-the-art injury criteria for the head.

Table 3. Injury criteria for the head under blunt sagittal loading – state-of-the-art injury criteria

Criterion Nomenclature	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
HBac1	Linear combination of HIC ₃₆ and angular velocity [10]	Strain < 0.004718Δω + 0.000224HIC ₃₆	 Strain calculated from FEA and derived a linear combination relating angular velocity and HIC to strain Surface plot shown in figure 18, pg. 18 of [10] 	FEA
HBac2	BRIC [11]	$BRIC = \omega_{max}/\omega_{cr} + \alpha_{max}/\alpha_{cr}$ Linearized CSDM and HIC were used to obtain risk curves related to BRIC (pg. 5-6 of [11]) $BRIC \text{ is roughly 1 for 50\%}$ AIS 3+	• Authors note that BRIC is not an "ultimate" head injury criterion that captures all possible brain injuries and skull fractures, but rather a correlation to TBI with head rotation being a primary injury mechanism. Also, They mention that using HIC and BRIC together might offer better performance	ATD and FEA
HBac3	BrIC [12]	$BrIC = sqrt((\omega_x/\omega_{xc})^2 + (\omega_y/\omega_{yc})^2 + (\omega_z/\omega_{zc})^2)$ $BrIC = 2 \text{ for } 50\% \text{ AIS} + \text{risk}$ (See curves pg. 310 of [12])	 Similar to BRIC. However, it is not known whether BrIC is meant to be a replacement of BRIC Original development of BrIC cited BrIC = 1.08 for 50% AIS3+ risk [13] 	ATD and FEA
HBac4	RIC [14]	RIC ₃₆ = 1.03x10^7 for 50% risk of MTBI RIC= $[(t_2-t_1)$ $(\frac{1}{(t_2-t_1)}) \int_{t_1}^{t_2} \alpha(t)dt)^{2.5}]_{max}$	Authors propose to use RIC, PRHIC, and HIC in conjunction	HIC

Criterion Nomenclature	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
HBac5	PRHIC [14]	PRHIC ₃₆ = 8.70x10^5 for 50% risk of MTBI PRHIC= $[(t_2-t_1)]$ $(\frac{1}{(t_2-t_1)}) \int_{t_1}^{t_2} \text{HIP_rot} dt)^{2.5}]_{\text{max}}$	Authors propose to use RIC, PRHIC, and HIC in conjunction	HIC and HIP
HBac6	Blunt criterion (BC) for skull fracture [15]	F = 5970 N for 50% risk BC = 1.61 for 50% risk Strain = 0.51% for 50% risk $BC = ln \frac{0.5mV^2}{M^{1/3}TD}$	• <i>m</i> is the mass of the projectile, <i>V</i> the velocity of the projectile, <i>M</i> the mass of the struck individual, <i>T</i> the combined thickness of the soft tissue and skull at the impact location, and <i>D</i> the diameter of the projectile	PMHS
HBac7	Skull Fracture Correlate [16][17]	$SFC = A_{HIC} = \Delta V_{HIC}/\Delta T_{HIC}$ $SFC < 120g \ for \ skull \ fracture$ probability less than 15%		PMHS and ATD
HBac8	Combined probability of concussion (CP) [18]	CP contours are provided in figure 2 of [18] CP = 0.5 (i.e. $a \approx 120g$ and $\alpha \approx 7000 \text{ rads/s}^2$) for 50% risk $CP = \frac{1}{1 + e^{-(\beta_0 + \beta_1 a + \beta_2 \propto + \beta_3 a\alpha)}}$	 A concussion risk function was developed from football players' dataset using a multivariate logistic regression analysis β0, β1, and β2 are regression coefficients, a is peak linear acceleration, α is peak rotational acceleration 	Human dataset
HBac9	Injury risk vs. ΔV [19]	See figures 2 and 4 in [19] for AIS 2+ curves in various regions $\Delta V \approx 95 \text{ km/h for } 50\% \text{ head injury risk belted AIS } 2+$	• Provides injury risk (AIS 2+ vs ΔV) for most regions of the body for belted and unbelted cases	Human dataset

State-of-the-Art Injury Research

Table 4 provides a summary of sagittal state-of-the-art injury research.

Table 4. Injury criteria for the head under blunt sagittal loading – state-of-the-art injury research

Criterion Nomencl ature	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
HBar1	Shear stress [20]	7.8 kPa for 50% risk of MTBI	Reference also provides angular velocity risk curves	ATD and FEA
HBar2	VM strain, VM stress, and First principal strain for DAI [21] CSF pressure for SDH [21] Skull strain energy for skull fracture [21]	VM strain = 25% Mild DAI, 35% Severe DAI First strain = 31% Mild DAI, 40% Severe DAI VM Stress(kPa) = 26 Mild DAI, 33 Severe DAI CSF pressure = -135 kPa for SDH Skull strain energy = 865 mJ for skull fracture All limits are for 50% risk	• Injury metrics were taken from the ULP FEM	FEA
HBar3	Axonal strain [22]	Axonal strain = 0.1565 for 50% risk of DAI	• Seems to have good correlation with DAI; axonal strain AUROC=0.988, axonal strain rate AUROC=0.889	FEA
HBar4	Principal component score [23]	PCS = 10((.4718*sGSI + .4742*sHIC + .4336*sLIN + .2164*sROT) + 2) Where sX=(X-mean(X))/(SD(X))	 Combination of other injury criteria values in one equation PCS can be multiplied by a coefficient to adjust for impact location 	Other injury metrics

CORONAL LOADING

Regulatory

Table 5 provides a summary of blunt head injury criteria currently in use by regulatory agencies.

Table 5. Injury criteria for the head under blunt coronal loading – regulatory

Criterion Nomenclature	Injury Criterion	Agencies
HBr3	HIC HIC = 390 to 1000 (depending on version and regulation)	FAA [2] NHTSA [24] ECE [25] Japan NCAP [5] IIHS [26] Euro NCAP [7]
HBr4	Resultant acceleration of head form cannot exceed 72g for more than 3 ms	Euro NCAP [7]
HBr5	Contact surface covered with ≥ 2 in padding (recommendation)	FAA (Special Condition) [27]

Table 6 provides a summary of penetrating head injury criteria currently in use by regulatory agencies.

Table 6. Injury criteria for the head under penetrating coronal loading – regulatory

Criterion Nomenclature	Injury Criterion	Agencies
HPr2	Areas of contact free of protrusions or sharp edges	FAA [8] NHTSA [9]

State-of-the-Art Injury Criteria

Table 7 provides a summary of coronal state-of-the-art injury criteria.

Table 7. Injury criteria for the head under blunt coronal loading – state-of-the-art injury criteria

Criterion Nomencl ature	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
HBac10	Linear combination of HIC ₃₆ and angular velocity [10]	Strain < 0.004718Δω + 0.000224HIC ₃₆	 Strain calculated from FEA and derived a linear combination relating angular velocity and HIC to strain Surface plot shown in figure 18, pg. 18 of [10] 	FEA

Criterion Nomencl ature	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
HBac11	BRIC [11]	$BRIC = \omega_{max}/\omega_{cr} + \alpha_{max}/\alpha_{cr}$ Linearized CSDM and HIC were used to obtain risk curves related to BRIC (pg. 5-6 of [11]) $BRIC \approx 1 \text{ for } 50\% \text{ AIS } 3+$	• Authors note that BRIC is not an "ultimate" head injury criterion that captures all possible brain injuries and skull fractures, but rather a correlation to TBI with head rotation being a primary injury mechanism. Also, they mention that using HIC and BRIC together might offer better performance	ATD and FEA
HBac12	BrIC [12]	BrIC=sqrt($(\omega_x/\omega_{xc})^2+(\omega_y/\omega_{yc})$ $^2+(\omega_z/\omega_{zc})^2$) BrIC = 2 for 50% AIS3+ risk (See curves pg. 310 of [12])	 Similar to BRIC. However, it is not known whether BrIC is meant to be a replacement of BRIC Original development of BrIC cited BrIC = 1.08 for 50% AIS3+ risk [13] 	ATD and FEA
HBac13	RIC [14]	RIC36 = 1.03x10^7 for 50% risk of MTBI RIC= $[(t_2-t_1)]$ $\left(\frac{1}{(t_2-t_1)}\right) \int_{t_1}^{t_2} \alpha(t)dt)^{2.5}]_{\text{max}}$	• Authors propose to use RIC, PRHIC, and HIC in conjunction	НІС
HBac14	PRHIC [14]	PRHIC36 = 8.70x10^5 for 50% risk of MTBI PRHIC= $[(t_2-t_1)] (t_2-t_1) \int_{t_1}^{t_2} HIP_rot dt)^{2.5} \Big]_{max}$	• Authors propose to use RIC, PRHIC, and HIC in conjunction	HIC and HIP
HBac15	Peak contact force and work [28]	Contact F = 1800 N for 50% Face fracture (AIS1+) Contact F = 4700 N for 50% vault fracture (AIS2+)	• Risk curves vs. deformation work given on pg. 7 [28]	PMHS
HBac16	Blunt criterion (BC) for skull fracture [15]	F = 5970 N for 50% risk BC = 1.61 for 50% risk Strain = 0.51% for 50% risk $BC = ln \frac{0.5mV^2}{M^{1/3}TD}$	• <i>m</i> is the mass of the projectile, <i>V</i> the velocity of the projectile, <i>M</i> the mass of the struck individual, <i>T</i> the combined thickness of the soft tissue and skull at the impact location, and <i>D</i> the diameter of the projectile	PMHS

Criterion Nomencl ature	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
HBac17	Skull Fracture Correlate [16][17]	$SFC = A_{HIC} = \Delta V_{HIC}/\Delta T_{HIC}$ $SFC < 120g \ for \ skull \ fracture$ probability less than 15%		PMHS and ATD
HBac18	Combined probability of concussion (CP) [18]	CP contours are provided in fig. 2 of [18] CP = 0.5 (i.e. $a \approx 120g$ and $\alpha \approx 7000$ rads/s^2) for 50% risk $CP = \frac{1}{1 + e^{-(\beta_0 + \beta_1 a + \beta_2 \propto + \beta_3 a\alpha)}}$	 A concussion risk function was developed from football players' dataset using a multivariate logistic regression analysis β0, β1, and β2 are regression coefficients, a is peak linear acceleration, a is peak rotational acceleration 	Human dataset

State-of-the-Art Injury Research

Table 8 provides a summary of coronal state-of-the-art injury research.

Table 8. Injury criteria for the head under blunt coronal loading – state-of-the-art injury research

Criterion Nomencl ature	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
HBar5	Shear stress [19]	7.8 kPa for 50% risk of MTBI	Reference also provides angular velocity risk curves	ATD and FEA
HBar6	VM strain, VM stress, and First principal strain for DAI [21] CSF pressure for SDH [21] Skull strain energy for skull fracture [21]	VM strain = 25% Mild DAI, 35% Severe DAI First strain = 31% Mild DAI, 40% Severe DAI VM Stress(kPa) = 26 Mild DAI, 33 Severe DAI CSF pressure = -135 kPa for SDH Skull strain energy = 865 mJ for skull fracture	• Injury metrics were taken from the ULP FEM	FEA

Criterion Nomencl ature	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
		All limits are for 50% risk		
HBar7	Axonal strain [22]	Axonal strain = 0.1565 for 50% risk of DAI	• Seems to have good correlation with DAI; axonal strain AUROC = 0.988, axonal strain rate AUROC = 0.889	FEA
HBar8	Principal component score [23]	PCS = 10((.4718*sGSI + .4742*sHIC + .4336*sLIN + .2164*sROT) + 2) Where sX = (X-mean(X))/(SD(X))	 Combination of other injury criteria values in one equation PCS can be multiplied by a coefficient to adjust for impact location 	Other injury metrics

INJURY CRITERIA FOR THE NECK

SAGITTAL LOADING

Regulatory

Table 9 provides a summary of blunt neck injury criteria currently in use by regulatory agencies.

Table 9. Injury criteria for the neck under blunt sagittal loading – regulatory

Criterion Nomenclature	Injury Criterion	Agencies
	Peak tension, compression, and shear	NHTSA [3] Japan NCAP [5]
NBr1	(compression applies to NHTSA and IIHS only and shear applies to	IIHS [6]
	Euro and Japan NCAP only)	Euro NCAP [7]

Criterion Nomenclature	Injury Criterion	Agencies
NBr2	N_{ij}	NHTSA [3] IIHS [6] FAA (Special Condition) [40] ¹
NBr3	NII	ISO 13232-5 [29]
NBr4	NIC	ECE [4] Euro NCAP [7]
NBr5	Bending moment	ECE [4] Japan NCAP [5] Euro NCAP [7]
NBr6	N _{km} (whiplash)	Euro NCAP [7]
NBr7	Head rebound velocity (whiplash)	Euro NCAP [7]
NBr8	T1-vertebra x-acceleration (whiplash)	Euro NCAP [7]
NBr9	Head restraint contact time (whiplash)	Euro NCAP [7]
NBr10	Max seat deflection (for high pulse) (whiplash)	Euro NCAP [7]

Table 10 provides a summary of Penetrating Neck Injury Sagittal Loading - Regulatory.

Table 10. Injury criteria for the neck under penetrating sagittal loading – regulatory

Criterion Nomenclature	Injury Criterion	Agencies
NPr1	Areas of contact free of protrusions or sharp edges	FAA [8] NHTSA [9]

State-of-the-Art Injury Criteria

Table 11 provides a summary of Neck state-of-the-art injury criteria.

Table 11. Injury criteria for the neck under blunt sagittal loading – state-of-the-art injury criteria

 $^{^{1}}$ N_{ij} has been applied to oblique seats by FAA Special Condition. While these seats are considered side-facing, N_{ij} evaluates sagittal loading, not coronal loading.

Criterion Nomenclature	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
NBac1	MIX [30]	MIX= $ \sqrt{\left(\frac{NIC_{max}}{NIC_{av}}\right)^{2} + \left(\frac{N_{km}}{N_{av}}\right)^{2}} $ MIX ≈ 4.1 for 50% risk of AIS1+ with symptoms > 1 month	• Risk curve shown in figure 16 of [30]	N _{km} and NIC _{max}
NBac2	NII _{PMHS} [31]	$NII_{PMHS} = max \left(\left(\left(\left(\frac{F_C}{F_{CC}} \right)^2 + \left(\frac{Mx}{F_{Z_{Crit}}} \right)^2 + \left(\frac{Mext}{My_{crit}} \right)^2 \right)^2 + \left(\frac{Mext}{My_{crit}} \right)^2 \right)^{1/2} + \left(\frac{Mflx}{Mz_{crit}} \right)^2 \right)^{1/2}, 1.77 \left(\frac{F_C}{F_{CC}} + \frac{F_T}{F_{TC}} \right) \right)$ $NII_{PMHS} = 1.86 \text{ for 50% risk of AIS3+}$	Adaptation of NII	NII and PMHS
NBac3	MANIC(-Gx) [58]	N_{ij}	• Modified risk curves for AIS2+ and AIS3+ provided [58]	Human dataset
NBac4	Modified N _{ij} [33]	$Nij = \frac{Fz}{3880 N} + \frac{\sqrt{My^2 + Mx^2}}{155 Nm}$ $N_{ij} < 1 \text{ limit}$	Assumed similar injury characteristic for flexion and lateral bending	Nij
NBac5	Sum of the shearing displacement (SSD) at each intervertebral level [34]	$SSD = \sum_{i=1}^{7} C_i - C_{i+1} dx$ Where C are the vertebrae shearing displacement $SSD \approx 4.75 \text{ mm for } 50\% \text{ risk}$ of WAD3+	 Criterion does not seem to correlate very well with the data Risk curves for WAD1+, 2+, and 3+ shown in figure 27 of [34] Criterion for whiplash injury 	FEA

Criterion Nomenclature	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
NBac6	NDC [35]	 θoc < 50°, xoc-t1 < 70 mm and zoc-t1 < -35 mm for acceptable level (Hybrid III). θoc is the OC rotation, xoc-t1 and zoc-t1 are the displacements of T1 relative to OC 	 Guidelines are dependent on dummy used. Hybrid III and BioRID P3 guidelines were defined on the study See figures 7, 8 and tables VI, VII of [35] for the proposed guidelines 	Human subjects and ATD
NBac7	Injury risk vs ΔV [19]	See figures 2 and 4 in [19] for AIS 2+ curves in various regions $\Delta V \approx 97 \text{ km/h for } 50\%$ neck/spine injury risk belted AIS 2+	• Provides injury risk (AIS 2+ vs ΔV) for most regions of the body for belted and unbelted cases	Human dataset

State-of-the-Art Injury Research

Table 12 provides a summary of sagittal state-of-the-art injury research.

Table 12. Injury criteria for the neck under blunt sagittal loading – state-of-the-art injury research

Criterion Nomencla ture	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
NBar1	ΔV [36]	ΔV=2.3 m/s for 15% risk of serious injuryΔV=4.2 m/s for 50% risk of serious injury	• Authors note that more data is needed in the 2-4 m/s head velocity	PMHS
NBar2	WIC [37]	WIC = Myoc-Mlw Myoc = moment about OC Mlw = moment measured at the T1 load cell	No tolerance limits providedCriterion for whiplash injury	ATD
NBar3	LNL – Index [38]		 Lower moments measured at a different vertebra than the one intended (T1) No tolerance limits provided 	ATD

CORONAL LOADING

Regulatory

Table 13 provides a summary of blunt neck injury criteria currently in use by regulatory agencies.

Table 13. Injury criteria for the neck under blunt coronal loading – regulatory

Criterion Nomenclature	Injury Criterion	Agencies
NBr11	Peak tension, compression, and shear (shear applies to FAA only)	FAA [39] IIHS [26]
NBr12	Bending moment	FAA [39]
NBr13	Rotation of head relative to torso (oblique seat)	FAA (Special Condition) [40]
NBr14	No concentrated loading from contact (oblique seat)	FAA (Special Condition) [40]
NBr15	Contact surface covered with ≥ 2 in padding (recommendation)	FAA (Special Condition) [27]

Table 14 provides a summary of Penetrating Neck Injury Coronal Loading Regulatory.

Table 14. Injury criteria for the neck under penetrating coronal loading – regulatory

Table 14 Hijary	criteria for the neek ander penetrating ed	Tonai loading Tegalatory
Criterion Nomenclature	Injury Criterion	Agencies
NPr2	Areas of contact free of protrusions or sharp edges	FAA [8] NHTSA [9]

State-of-the-Art Injury Criteria

Table 15 provides a summary of Neck state-of-the-art injury criteria.

Table 15. Injury criteria for the neck under blunt coronal loading – state-of-the-art injury criteria

Criterion Nomenclature	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
NBac8	MANIC(Gy) [32]	MANIC(Gy)= $ \left(\frac{Fx}{Fx_{crit}}\right)^{2} + \left(\frac{Fy}{Fy_{crit}}\right)^{2} + \left(\frac{Fz}{Fz_{crit}}\right)^{2} + \left(\frac{My}{My_{crit}}\right)^{2} + \left(\frac{Mz}{Mz_{crit}}\right)^{2} $ MANIC(Gy) = 0.473 for 5% risk of AIS 2+	• Risk curves for AIS2+ and AIS3+ provided in figure 5, pg.160 of [32]	Human dataset
NBac9	IV-NIC [41]	$IV - NICi, j(t)$ $= \frac{\theta_{dynamic, i, j}(t)}{\theta_{physiological, i, j}}$ $IV-NIC injurious threshold = 1.5-4.0 Depending on intervertebral level$	Does not provide risk curves	PMHS
NBac10	Modified Nij [33]	$Nij = \frac{Fz}{3880 N} + \frac{\sqrt{My^2 + Mx^2}}{155 Nm}$ $Nij < 1 \text{ limit}$	Assumed similar injury characteristic for flexion and lateral bending	Nij

State-of-the-Art Injury Research

Table 16 provides a summary of coronal state-of-the-art injury research.

Table 16. Injury criteria for the neck under blunt coronal loading – state-of-the-art injury research

Criterion Nomencl ature	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
NBar4	LNL – Index [38]	$LNL = \left \frac{\sqrt{My_{lower}^2 + Mx_{lower}^2}}{C_{moment}} \right + \left \frac{\sqrt{Fx_{lower}^2 + Fy_{lower}^2}}{C_{shear}} \right + \left \frac{Fz_{lower}}{C_{tension}} \right $	 Lower moments measured at a different vertebra than the one intended (T1) No tolerance limits provided 	ATD

INJURY CRITERIA FOR THE TORSO

SAGITTAL LOADING

Regulatory

Table 17 provides a summary of blunt thorax injury criteria currently in use by regulatory agencies.

Table 17. Injury criteria for the torso under blunt sagittal loading – regulatory

Criterion Nomenclature	Injury Criterion	Agencies
TBr1	Acceleration of thoracic instrumentation cannot exceed 60g for more than 3 ms	NHTSA [3] Japan NCAP [5] IIHS [6]
TBr2	Compressive deflection of the sternum relative to the spine (ThCC)	NHTSA [3] ECE [4] IIHS [6] Euro NCAP [7]
TBr3	Chest deflection	Japan NCAP [5]
TBr4	Viscous Criterion (VC)	ECE [4] IIHS [6] Euro NCAP [7]
TBr5	Sternum deflection rate	IIHS [6]
TBr6	No submarining	FAA [2] Japan NCAP [5]
TBr7	Load in shoulder harness straps	FAA [2]

Criterion Nomenclature	Injury Criterion	Agencies
TBr8	Lumbar load	FAA [2]

Table 18 provides a summary of Penetrating Thoracic Injury Sagittal Loading in use by regulatory agencies.

Table 18. Injury criteria for the torso under penetrating sagittal loading – regulatory

Criterion Nomenclature	Injury Criterion	Agencies
TPr1	Areas of contact free of protrusions or sharp edges	FAA [8] NHTSA [9]

State-of-the-Art Injury Criteria

Table 19 provides a summary of Thorax state-of-the-art injury criteria.

Table 19. Injury criteria for the torso under blunt sagittal loading – state-of-the-art injury criteria

Ci4i		Tolonomas	same or the first injury critical	Daning 1
Criterion Nomenclature	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
TBac1	Combined deflection (Dc) [42]	Dc = Ds + Cf[(dD - Lc) + (dD - Lc)] $- Lc)]$ $Dc < 65 mm for 50% risk of 6+ rib fracture$	 Risk curves shown in figures 12 of [42] Moderate restraint dependency 	FEA
TBac2	Maximum chest deflection (C _{max}) [43]	C _{max} ~ 37% for 50% risk of 6+ rib fracture (60 year old male)	Risk curves shown in figures4-5 of [43]Age sensitive	PMHS and FEA
TBac3	Equivalent deflection (d _{eq}) [44]	$d_{eq}(t) = (d_1^2(t) + f_n d_d(t)^2)^{(1/2)}$ $d_{eq} \approx 32 \text{ mm for 50\% AIS3+}$ risk	 ASI3+ risk curve in figure 22, pg. 338 of [44]. In addition, it presents belt only, airbag only, combined, and all restraints risk curves for other criteria (VC, CTI, sternum deflection). Risk curves were modified to include age effects 	FEA, PMHS, and ATD
TBac4	Injury risk vs ΔV [19]	See figures 2 and 4 in [19] for AIS 2+ curves in various regions	• Provides injury risk (AIS 2+ vs ΔV) for most regions of the body for belted and unbelted cases	Human dataset

Criterion Nomenclature	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
		$\Delta V \approx 80$ km/h for 50% thorax injury risk belted AIS 2+		
TBac5	Eiband [59]	See figure 3 in [59]	• Human volunteers tolerated 10 G for 0.1 seconds and 15 G for 0.05 seconds	Human volunteer and animal data
TBac6	DRI [60]	See details in [60]	•DRI of 19 is approximately a 9% risk of a detectable spinal injury	Human dataset

State-of-the-Art Injury Research

Table 20 provides a summary of sagittal state-of-the-art injury research.

Table 20. Blunt Lower Extremities State-of-the-Art Research Sagittal Loading

Criterion Nomencl ature	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
TBar1	Pelvis Loads [45]	-	A literature review itselfProvides tolerance limits from other papers	N/A
TBar2	Pelvis Loads [46]	Peak axial force injury tolerance 6.1 kN (AIS 2+)	-	PMHS
TBar3	Hip joint load [47]	Neutral posture fracture tolerance ~5.7-6.1 kN	• Tolerance load decreases 1.8% per degree of adduction & 1% per degree of flexion	PMHS

CORONAL LOADING

Regulatory

Table 21 provides a summary of blunt thorax injury criteria currently in use by regulatory agencies.

Table 21. Injury criteria for the torso under blunt coronal loading – regulatory

Table 21. Injury criteria for the torso under blunt coronal loading – regulatory			
Criterion Nomenclature	Injury Criterion	Agencies	
		NHTSA [24] FAA [39]	
TBr9	Rib deflection	IIHS [26]	
		ECE [25]	
		Euro NCAP [7]	
TBr10	Chest deflection	Japan NCAP [5]	
		ECE [25]	
TBr11	Viscous Criterion (VC)	Euro NCAP [7]	
		IIHS [26]	
TBr12	Thoracic Trauma Index (TTI)	NHTSA [24]	
		FAA[48] NHTSA [24]	
	Abdominal forces	FAA [39]	
TBr13		ECE [25]	
		Japan NCAP [5]	
TBr14	Rib deflection rate	IIHS [26]	
TBr15	Lateral flexion < 40°	FAA [39]	
TBr16	Rearward acceleration cannot exceed 20g for more than 3 ms (Oblique seats)	FAA (Special Condition) [40]	
TBr17	Contact surface covered with ≥ 2in padding (recommendation)	FAA (Special Condition) [27]	
TBr18	Load in shoulder harness straps	FAA [2]	
TBr19	Abdomen lateral compression	Euro NCAP [7]	
TBr20	Lumbar load	FAA [2]	
TBr21	Pelvic acceleration	FAA [8]	
		FAA [39]	
TBr22	Pubic symphysis force	NHTSA [24]	
11111111	i dole symphysis force	ECE [25]	
		Euro NCAP [7]	

Criterion Nomenclature	Injury Criterion	Agencies
		Japan NCAP [5]
TBr23	Load bearing portion of pelvis shall remain on the seat cushion (edge)	FAA [39]
TBr24	Resultant lower spine acceleration	NHTSA [24]
TBr25	Acetabular and iliac pelvic forces	NHTSA [24] IIHS [26]
TBr26	Shoulders remain aligned with the hips	FAA (Special Condition) [40]

Table 22 provides a summary of Penetrating Thorax Injury Coronal Loading in use by regulatory agencies.

Table 22. Injury criteria for the torso under penetrating coronal loading – regulatory

Criterion Nomenclature	Injury Criterion	Agencies
TPr2	Areas of contact free of protrusions or sharp edges	FAA [8] NHTSA [9]

State-of-the-Art Injury Criteria

None reported.

State-of-the-Art Injury Research

Table 23 provides a summary of sagittal state-of-the-art injury research.

Table 23. Injury criteria for the torso under blunt coronal loading – state-of-the-art injury research

Criterion Nomencl ature	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
TBar4	Loading corridors [49]	Deflection, accelerations, and force corridors shown in figures 7-8 of [49]	 Several tests with different wall configuration (i.e. padded, rigid, and offset) Small females in side impacts 	PMHS

INJURY CRITERIA FOR THE UPPER EXTREMITIES

SAGITTAL LOADING

Regulatory

Table 24 provides a summary of blunt upper extremities injury criteria currently in use by regulatory agencies.

Table 24. Injury criteria for the upper extremities under blunt sagittal loading – regulatory

Criterion Nomenclature	Injury Criterion	Agencies
UBr1	Humerus mid-shaft bending moment (upper arm)	IARVs [50]
UBr2	Ulna mid-shaft bending moment (forearm)	IARVs [50]

State-of-the-Art Injury Criteria

Table 25 provides a summary of sagittal state-of-the-art injury criteria.

Table 25. Injury criteria for the upper extremities under blunt sagittal loading – state-of-the-art injury criteria

Criterion Nomenclature	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
UBac1	Forearm Bending Tolerance [51]	Mean fracture force: 1860 N Mean bending moment to failure: 94 ± 41 Nm See figure 5 of [51] for graphed limits	• Slightly lower limit values at lower velocity tests, but not statistically different.	PMHS
UBac2	Humerus Limits [52]	50th percentile limits: Fx = Fy = 2.5 kN Mx = My = 230 Nm	-	PMHS
UBac3	Forearm Bending Tolerance [53]	At 3 m/s: Fracture Force $1386 \pm 198 \text{ N}$ Bending moment $88.9 \pm 12.6 \text{ Nm}$	-	PMHS
UBac4	Injury risk vs ΔV [19]	See figures 2 and 4 in [19] for AIS 2+ curves in various regions $\Delta V \approx 85 \text{ km/h for } 50\% \text{ upper extremities injury risk belted}$ AIS 2+	• Provides injury risk (AIS 2+ vs ΔV) for most regions of the body for belted and unbelted cases	Human dataset

State-of-the-Art Injury Research

None reported.

CORONAL LOADING

Regulatory

Table 26 provides a summary of blunt upper extremities injury criteria currently in use by regulatory agencies.

Table 26. Injury criteria for the upper extremities under blunt coronal loading – regulatory

			-
Criterion	Injury Criterion	Agencies	
Nomenclature	J. J.	8	

UBr3	Shoulder deflection	IIHS [26] IARVs [50]
UBr4	Lateral shoulder load	Euro NCAP [7] IARVs [50]
UBr5	Humerus mid-shaft bending moment (upper arm)	IARVs [50]
UBr6	Ulna mid-shaft bending moment (forearm)	IARVs [50]

State-of-the-Art Injury Criteria

Table 27 provides a summary of Upper Extremities state-of-the-art injury criteria.

Table 27. Injury criteria for the upper extremities under blunt coronal loading – state-of-the-art injury criteria

Criterion Nomenclature	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
		Mean fracture force:		
		1860 N		
UBac5	Forearm Bending	Mean bending moment to failure:	• Slightly lower limit values at lower velocity tests, but not	PMHS
	Tolerance [51]	94 ± 41 Nm	statistically different.	11/1110
		See figure 5 of [51] for graphed limits		
		50th percentile limits:		
UBac6	Humerus Limits [52]	Fx = Fy = 2.5 kN	-	PMHS
		Mx = My = 230 Nm		
		At 3 m/s:		
UBac7	Espanya Dan din s	Fracture Force		
	Forearm Bending Tolerance [53]	$1386 \pm 198 \text{ N}$	-	PMHS
		Bending moment		
		88.9 ± 12.6 Nm		

INJURY CRITERIA FOR THE LOWER EXTREMITIES

SAGITTAL LOADING

Regulatory

Table 28 provides a summary of blunt lower extremities injury criteria currently in use by regulatory agencies.

Table 28. Injury criteria for the lower extremities under blunt sagittal loading – regulatory

Table 28. Injury criteria for the lower extremities under blunt sagittal loading – regulator			
Criterion Nomenclature	Injury Criterion	Agencies	
		NHTSA [3]	
		ECE [4]	
LBr1	Earny force oritorion (EEC)	Euro NCAP [7]	
LDII	Femur force criterion (FFC)	Japan NCAP	
		IIHS [6]	
		FAA [2]	
		ECE [4]	
LBr2	Tibia compression force criterion (TCFC)	Euro NCAP [7]	
	(Tere)	IIHS [6]	
		ECE [4]	
LBr3	Tikio index (TI)	Euro NCAP [7]	
LDIS	Tibia index (TI)	Japan NCAP [5]	
		IIHS [6]	
		ECE [4]	
LBr4	Movement of sliding knee joints (tibia-femur displacement)	Euro NCAP [7]	
	(cross remai displacement)	IIHS [6]	
I D.,5	Dodol moomyoud displacement	Euro NCAP [7]	
LBr5	Pedal rearward displacement	Japan NCAP [5]	
LBr6	Foot acceleration	IIHS [6]	
LBr7	KTH criterion	IIHS [6]	

State-of-the-Art Injury Criteria

Table 29 provides a summary of sagittal state-of-the-art injury criteria.

Table 29. Injury criteria for the lower extremities under blunt sagittal loading – state-of-the-art injury criteria

Criterion Nomenclature	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
LBac1	Plantar foot load [54]	9.1 kN for 50% risk of any foot-ankle injury (50 years) Other probability levels provided in tables 2-4 of [54].	• Provides risk curves for 3 Groups of fracture; all footankle, any calcaneus, and any tibia injury	PMHS
LBac2	Plantar flexed-foot load [55]	3.3 kN for 50% risk of foot injury See table 3 and figures 6-8 of [55] for other thresholds	-	PMHS
LBac3	Ankle malleolus injury criterion [56]	50 Nm dorsiflexion for 25% risk of ankle malleolus injury 33 Nm eversion for 25% risk of Ankle malleolus injury	-	Human dataset
LBac4	Injury risk vs ΔV [19]	See figures 2 and 4 in [19] for AIS 2+ curves in various regions $\Delta V \approx 75 \text{ km/h for } 50\% \text{ lower extremities injury risk belted}$ AIS 2+	• Provides injury risk (AIS 2+ vs ΔV) for most regions of the body for belted and unbelted cases	Human dataset

State-of-the-Art Injury Research

None reported.

CORONAL LOADING

Regulatory

Table 30 provides a summary of blunt lower extremities injury criteria currently in use by regulatory agencies.

Table 30. Injury criteria for the lower extremities under blunt coronal loading – regulatory

Criterion Nomenclature	Injury Criterion	Agencies
LBr8	Leg flail < 35°	FAA [39]

Criterion Nomenclature	Injury Criterion	Agencies
LBr9	Femur force and bending moment	IIHS [26]

State-of-the-Art Injury Criteria

Table 31 provides a summary of coronal state-of-the-art injury criteria.

Table 31. Injury criteria for the lower extremities under blunt coronal loading – state-of-the-art injury criteria

Criterion Nomenclature	Injury Criterion	Tolerance Limits/Criteria	Comments	Derived from
LBac5	Plantar Foot Load [54]	9.1 kN for 50% risk of any foot-ankle injury (50 years)Other probability levels given in table 2-4 of [54].	• Provides risk curves for 3 Groups of fracture; all footankle, any calcaneus, and any tibia injury	PMHS
LBac6	Knee Injury Criterion [57]	$\begin{split} D_{shearing} &= \text{-}0.054*B^2_{bending} \text{ -} \\ 0.62*B_{bending} &+ 25 \\ \text{for } B_{bending} &\geq 9^\circ \\ \\ D_{shearing} &= 15 \text{ mm} \\ \text{for } B_{bending} \text{ between } 0^\circ \text{ and } 9^\circ \end{split}$	-	PMHS and FEA

State-of-the-Art Injury Research

None reported.

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